

Applications of the Boltzmann Equation I.

→ Chapman - Enskog \rightsquigarrow Basics (C-E Light)

- a major application of B.E. is calculation of transport coeffs.

- recall, fluid equations involve momentum, heat flux

i.e. really $\frac{\partial \underline{v}}{\partial t} = - \nabla \cdot \underline{\Pi}$, etc.

continuity form

here:

$$\Pi_{\alpha, \beta} = mn (U_\alpha V_\beta + \langle U'_\alpha V'_\beta \rangle)$$

$$\langle U'_\alpha V'_\beta \rangle = \int f^3 v f U'_\alpha V'_\beta$$

$$\text{if } f = f_0 = \frac{n(x)}{(2\pi)^{3/2} V_{Th}(x)^3} \exp \left[- \frac{(v - v(x))^2}{2 V_{Th}^2} \right]$$

\Rightarrow

$$\langle U'_\alpha V'_\beta \rangle = \frac{2}{3} \langle v^2 \rangle \delta_{\alpha, \beta}$$

$$\langle v^2 \rangle = 3T/m$$

but $\hat{f} \hat{f} \hat{f} \hat{f} \hat{f} \hat{f} \hat{f}$ $f = f_0 \hat{P} \hat{P} \hat{P}$

21

Recall, f satisfies:

$$\partial_t f + \underline{v} \cdot \underline{\nabla} f = C(f)$$

$\Rightarrow f_0$ cannot solve B.E. unless $\nabla f_0 = 0$

can assign time scales:

$$\partial_t f \rightarrow \omega$$

$$\underline{v} \cdot \underline{\nabla} f \rightarrow v_{th}/L$$

{Collisional regime
 $h \ll \tau > \frac{v_{th}}{\omega}$ }

$$C(f) \rightarrow \tau ; \quad \tau = \frac{v_{th}}{l_{mfp}}$$

$\Rightarrow f_0$ is 0th Order solution.

$$l_{mfp} = 1/n\tau$$

then if f_0 is homogeneous \Rightarrow stationary solution,
 $h \ll$ correction

$$f = f_0 + \delta f$$

$\hookrightarrow \sim$ inhomogeneity! \rightarrow more precisely
response to
inhomogeneity
i.e. $\nabla T, \nabla V$

$$\text{and } \langle \dot{V}_A' V_B' \rangle = \int d^3V \left(f_0 + \delta f \right) V_A' V_B'$$

$$= P_{A,B}^{\delta f} + \overset{\uparrow}{\text{Viscous stress}}$$

$$\text{viscosity} \sim mn D \quad \underline{\underline{M}}$$

$$\text{d.e. } mn \langle v'_x v'_y \rangle_{v_{loc}} = -\eta \frac{d \langle v_x \rangle}{dx_y} + \dots \quad D \sim \text{length}$$

\hookrightarrow generic form of
viscous stress

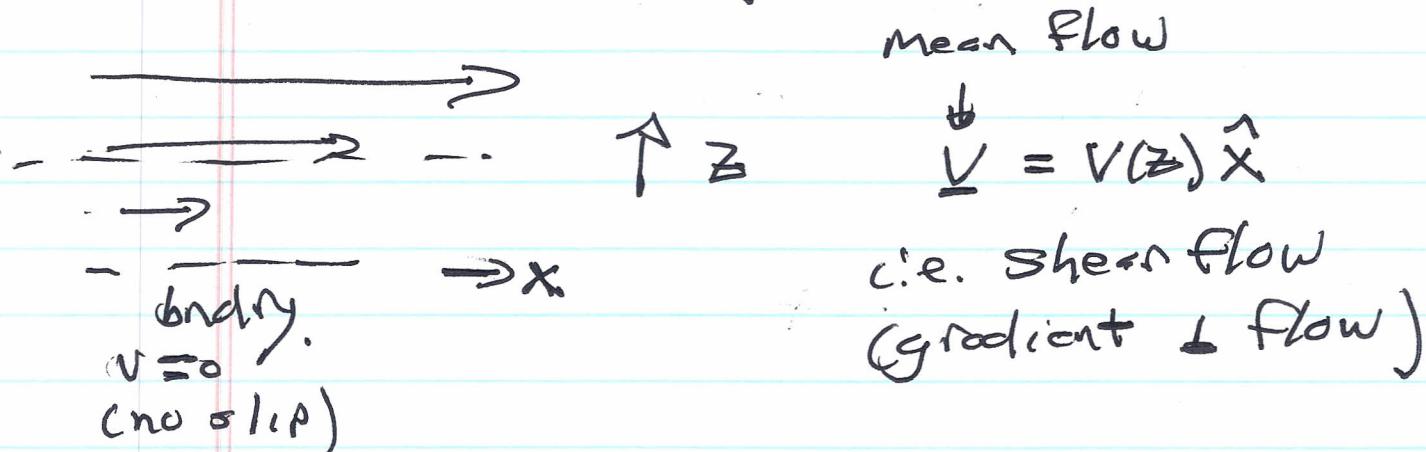
∞ , need:

- understand viscosity, etc.
- see how calculate if any
then transport coeffs (viscosity)

∞ What is viscosity about?

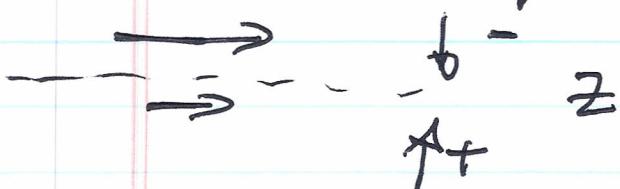
- simple physics of transport coeffs:

Consider collisional gas:



i.e. shear flow
(gradient ⊥ flow)

choose imaginary surface



Calculate transport of \hat{x} momentum thru surface:

$$\Pi_+ = \int_{V_z > 0} d\mathbf{v} m V_x V_z f$$

$$\sim V_m V \Delta M +$$

$$\Pi_- = \int_{V_z < 0} d\mathbf{v} m V_x V_z f$$

at first glance, would appear $\Pi_+ = \Pi_-$

so $\Pi_{tot} = 0$ but:

$$- - - \Rightarrow \overline{\text{f}} \text{mfp}$$

\rightarrow "scale of resolution" for imaginary surface is fmfp \Rightarrow defines effective thickness.

\rightarrow "V(z) has gradient across this"

$$\stackrel{\infty}{=} \Pi_{tot} = \Pi_- + \Pi_+$$

Ω Π_-

$$\Pi \approx -nm v_{th} \bar{V} \left(z + \frac{l_{max}}{2} \right) \\ + nm v_{th} \bar{V} \left(z - \frac{l_{max}}{2} \right)$$

$$\Pi_+$$

$$\approx -nm v_{th} l_{max} \frac{\partial \bar{V}}{\partial z} \\ \rightarrow \sim l_{max} v_{th}$$

$$\approx -nm D \frac{\partial \bar{V}}{\partial z}$$

$$= -\eta \frac{\partial \bar{V}}{\partial z}$$

↓
viscosity (shear)
 $\sim \rho D$

→ Key Points:

- equal # collisions, kicks in +, - directions, but
- more momentum kicked down from above, due velocity gradient.
- ⇒ net viscous momentum transport via collisions to relax gradient

How calculate systematically?

⇒ Chapman - Enskog expansion!

now

$$\frac{\partial f'}{\partial t} + \underline{v} \cdot \underline{\nabla} f = \text{c.c.e.}$$

\downarrow

$\frac{v_{\text{th}}}{L}$

{ multiple
time
scales

$v_{\text{eff.}}$

f norm to n

and seek:

$$\Pi_{z,x} = \int d^3 v \, v_z \, (m v_x f)$$

\downarrow

\vec{z} direction flux
of \vec{x} momentum

$$f = f_0 + df$$

$$\Pi_{z,x} = \int d^3 v \, v_z \, (m v_x (f_0 + df))$$

$$\text{if } f_0 \approx \frac{n_0}{v_{\text{th}}^3} \exp \left[- \frac{(\underline{v} - \underline{v}(z) \hat{x})^2}{2 v_{\text{th}}^2 \alpha^2} \right]$$

(i.e. local Maxwellian)

Z.

→ f_0 contribution vanished by symmetry!

so

$$\Pi_{z,x} = \int d^3x \mathbf{v}_z \cdot (\mathbf{m} \cancel{\mathbf{v}_x}) \delta f$$

\uparrow
drives the flux.

How get δf ?

⇒ Perturbative solution?

$$\nabla \cdot \mathbf{f} = C(\mathbf{f}) \quad \rightarrow \quad \left. \begin{array}{l} \text{recursively} \\ \text{integral} \\ \text{equation!} \end{array} \right\}$$

L. O.: $C(\mathbf{f}) = 0$

$\mathbf{f} = \mathbf{f}_0 \rightarrow$ Local Maxwellian

1st O.:

$$\nabla \cdot \nabla \cdot \mathbf{f}_0 = C(\delta \mathbf{f})$$

$$\therefore \delta \mathbf{f} = C^{-1} [\nabla \cdot \nabla \cdot \mathbf{f}_0]$$

How?

→ lengthy calculation (comes)

→ Knock (creak) Mode

$$C(F) = -\nu (F - F_0)$$

$\frac{\partial}{\partial t}$
collisonal decay to
(loc.) Maxwellian
constant Energy

18

$$\underline{V} \cdot \underline{\nabla} F = C(F) = -\nu (F - F_0)$$

$$F = F_0 + \delta F$$

$$\underline{V} \cdot \underline{\nabla} (F_0 + \delta F) = -\nu (F - F_0)$$

$$d.o. -\nu (F - F_0) = 0$$

$$F = F_0$$

1st order

$$\underline{V} \cdot \underline{\nabla} F_0 = -\nu \delta F$$

$$\delta F = -\frac{\underline{V} \cdot \underline{\nabla}}{\nu} F_0$$

$\frac{\partial}{\partial t}$
perturbative
correction to F_0 ; $O\left(\frac{V_{th}}{L\nu}\right)$

9.

81

$$\begin{aligned} \Pi_{Z,x} &= \int d^3V \ v_z \ m v_x \ df \\ &= \int d^3V \ v_z \ n \ V_m v_x \left(-\frac{v_z}{r} \frac{\partial}{\partial z} f_0 \right) \end{aligned}$$

$$\bar{V}_x = V(z) \bar{x}$$

$$\begin{aligned} \text{now } f_0 &\approx \frac{n(x)}{V_{Th}(x)} \exp \left[-\frac{(v - \bar{V}(z)) \bar{x}}{2 V_{Th}^2(x)} \right] \\ &= \frac{n}{V_{Th}^3} \exp \left[-\frac{(v - \bar{V}(z))^2}{2 V_{Th}^2} \right] \end{aligned}$$

$$\frac{\partial f_0}{\partial z} = \frac{1}{V_{Th}^3} \frac{v_x}{V_{Th}^2} \frac{\partial \bar{V}(z)}{\partial z} \exp []$$

$$- 2 \frac{\bar{V}(z)}{V_{Th}^2} \frac{\partial \bar{V}(z)}{\partial z} \exp []$$

dropped \Rightarrow
 interested in only
 linear response
 of flux to
 gradient

see 9g

~~Velocity distribution function~~
~~Velocity distribution function~~

$$\frac{\partial f_0}{\partial z} = f_0 \frac{v_x}{V_{Th}^2} \frac{\partial \bar{V}(z)}{\partial z}$$

~~Velocity distribution function~~
~~Velocity distribution function~~

Note:

- here seek linear relation between flux and gradient
- assumes weak distortion from Maxwellian, i.e.

$$f_0 = \frac{n}{V_{Th}^3} \exp \left[-\frac{(v - v_B)^2}{2V_{Th}^2} \right]$$

$$= \frac{n}{V_{Th}^3} \exp \left[-\frac{v^2 - 2vV_{Th} + V^2}{2V_{Th}^2} \right]$$

$$\approx \frac{n}{V_{Th}} \exp \left[-\frac{v^2}{2V_{Th}^2} \right] \left[1 + \frac{v_x V}{V_{Th}^2} \right]$$

$$= f_0 \left(1 + \frac{v_x V}{V_{Th}^2} \right)$$

↑
e.o. factor on
 $\exp = 1 + x$

yields result.

88

$$\Pi_{zjx} = \int d^3x \ v_z m v_x \left(-\frac{v_z}{r} \frac{v_x}{v_{Th}^2} \right)$$

$$\leftarrow f_0 \frac{\partial V(z)}{\partial z}$$

$$= - \# \frac{m n}{r} v_{Th}^2 \frac{\partial V(z)}{\partial z}$$

$$= - \# m n \underbrace{\left(\frac{v_{Th}}{r} \right) v_{Th}}_{l_{MFP}} \frac{\partial V(z)}{\partial z}$$

$$D = v_{Th} l_{MFP}$$

$$\Pi_{zjx} = - \# m n D \frac{\partial V(z)}{\partial z}$$

$$= - \# \rho D \frac{\partial V(z)}{\partial z}$$

$$\eta = - \# \rho D$$

\Rightarrow basic result for collisions
viscosity ↓.

Note form of result:

$$\underline{\Gamma}_{z,x} = - \underbrace{\# nm/l}_{\text{macroscopic}} \frac{\partial V_x(z)}{\partial z}$$

↓
transport coefficient

→ gradient of thermo. quantity of (dist.)
thermodynamic force.

⇒ example of thermodynamic flux-force relation.

⇒ constitutive relation, proportionality is transport coefficient

In general, have vector relation:

$$\underline{\Gamma} = - \underline{\underline{K}} \cdot \underline{\nabla} C$$

↓
vector of fluxes | ↓
 vector of gradient

Matrix of transport coefficients = Onsager matrix
(n.b. Onsager symmetry → $\underline{\underline{K}}$ symmetric)

⇒ Observe:

- f_{\max} annihilates collision operator
eq.
and corresponds to $\frac{df}{dt} = 0$
state \rightarrow maximum entropy.

but

- $f_{\max}^{[n(x), T(x), V(x)]}$ does not
satisfy Boltzmann eqn. \Rightarrow of needed.

c.e. $\nabla \cdot \nabla f = C(f)$

$$\Rightarrow F = f_{\max} + \delta f$$

why: gradients in thermodynamic quantities, system is not in maximum entropy state
c.e. $\delta f \neq 0$

- so $\delta f \sim \nabla C$, \Rightarrow relaxation to maximum entropy state will occur by collisions/transport

- can describe relaxation macroscopically, i.e.

$$\Pi_{x,\alpha} = -\rho D \frac{\partial V_B}{\partial x_\alpha}$$

↑
Flux
↑
Force

- $\frac{\partial V_B}{\partial x_\alpha} \Pi_{x,\alpha} = \rho D \left(\frac{\partial V_B}{\partial x_\alpha} \right)^2$

$$\left\{ \frac{dS}{dt} = \frac{\rho D}{T} \left(\frac{\partial V_B}{\partial x_\alpha} \right)^2 \right.$$

— entropy production
due to transport
— induced relaxation

Note time scales:

c.) to form local Maxwellian,
H-thm. $\Rightarrow \tau_{coll} \sim \nu^{-1}$

d.) to form global ~~maximum~~ entropy state:

$$\begin{aligned} 1/\tau_{relax} &\sim D/L_v^2 \\ &\sim \nu \frac{L_{max}^2}{L_v^2} \end{aligned}$$

$$L_v^{-1} = \frac{1}{V} \frac{\partial V}{\partial x}$$

$$\tau_{\text{relax}} \sim (k v / \ell_{\text{MFP}})^2 \tau_{\text{coll.}}$$

\Rightarrow entropy production / relaxation is multiple time scale process!

More generally, can write:

$$J_i = - \sum_{j=1}^n \alpha_{ij} x_j^* \xrightarrow{\substack{\text{kinetic} \\ \text{coefficient}}} \xrightarrow{\substack{\text{driving} \\ \text{force}}} i^{\text{th}} \text{ flux}$$

$$\frac{dS}{dt} = \psi = \text{"Dissipation Function"}$$

$$\Rightarrow \frac{dS}{dt} = \sum_{i=1}^n \sum_{j=1}^n \alpha_{ij} x_i x_j$$

$$\text{c.e. } \frac{dS}{dt} = - x_j J_i$$

so, for 2x2:

$$\frac{dS}{dt} = \sum_{i=1}^2 \sum_{j=1}^2 \alpha_{ij} x_i^2 + (\alpha_{12} + \alpha_{21}) x_1 x_2 + \alpha_{32} x_2^2$$

clearly need:

$$\begin{aligned} \alpha_{1,1} &\geq 0 \\ \alpha_{2,2} &\geq 0 \end{aligned} \quad \rightarrow \text{i.e. diffusion down gradient}$$

and $\alpha_{1,1} \alpha_{2,2} - \frac{1}{4} (\alpha_{1,2} + \alpha_{2,1})^2 \geq 0.$

(i.e. descr \Rightarrow diag.)

N.B. off-diagonals?

i.e. can ∇T drive a density flux?

$$\Gamma = \int d^3v \mathbf{v} \cdot \delta f$$

$$\delta f = -\frac{1}{r} \mathbf{v} \cdot \nabla f_0$$

$$\Rightarrow \Gamma = \int d^3v \mathbf{v} \cdot \left(-\frac{1}{r} \mathbf{v} \cdot \frac{\partial}{\partial \mathbf{x}} \left(\frac{1}{V_m(\mathbf{x})^3} \exp \left[-\frac{m \mathbf{v}^2}{2T(\mathbf{x})} \right] \right) \right)$$

clearly can get contribution to Γ_x .
 \rightarrow Thermal diffusion.

Message: Gradient in distribution function
 is the key! --- but integration
 symmetric matter.